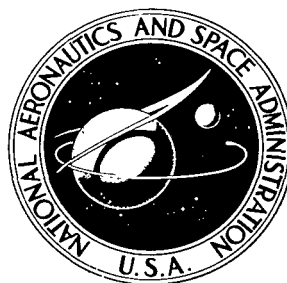
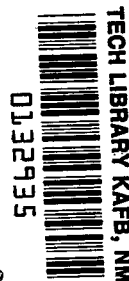


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VIBRATIONAL ENERGY TRANSFER IN  
EXPANDING MIXTURES OF  $N_2$  AND  $CO_2$   
AS MEASURED BY AN ELECTRON BEAM

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# VIBRATIONAL ENERGY TRANSFER IN EXPANDING MIXTURES OF N<sub>2</sub> AND CO<sub>2</sub> AS MEASURED BY AN ELECTRON BEAM

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## SUMMARY

The transfer of molecular vibrational energy was studied by means of the electron-beam technique in expanding mixtures of N<sub>2</sub> and CO<sub>2</sub> heated by an electric arc. High-temperature flowing N<sub>2</sub> was mixed in a plenum chamber with CO<sub>2</sub> at total pressures of 5 to 10 atm (507 to 1013 kN/m<sup>2</sup>) and total temperatures of 1500 to 4000 K and then expanded supersonically in a conical nozzle to free-stream conditions of about 0.05 mm Hg (7 N/m<sup>2</sup>) and 150 K. Vibrational temperatures of N<sub>2</sub> were measured in the expanded flow and compared with temperatures predicted by using a time-dependent technique for the numerical solution of the nonequilibrium flow. By means of this technique and the experimental data, the vibrational relaxation rates of expanding N<sub>2</sub> and CO<sub>2</sub> were deduced. The results indicate generally faster rates than those measured in shock tubes for the vibrational-translational exchange in N<sub>2</sub> and for the vibrational-vibrational exchange between the asymmetric stretching mode  $\nu_3$  and the bending mode  $\nu_2$  of CO<sub>2</sub>.

## INTRODUCTION

The near-resonant transfer of vibrational energy from N<sub>2</sub> to the asymmetric stretching mode  $\nu_3$  of CO<sub>2</sub>, illustrated in figure 1, has long been recognized as the process that makes N<sub>2</sub>-CO<sub>2</sub> laser action possible (ref. 1). As a result of considerable research effort on the N<sub>2</sub>-CO<sub>2</sub> molecular system (refs. 2 to 6) the general mechanisms involved are understood reasonably well, but the proper rate equations remain somewhat in doubt. The present objective is to measure directly the vibrational temperature of the N<sub>2</sub> molecules in a relaxing N<sub>2</sub>-CO<sub>2</sub> mixture in order to evaluate these rates. Vibrational relaxation times are deduced from the measured N<sub>2</sub> vibrational temperatures by using a time-dependent technique for the numerical solution of the nonequilibrium flow of N<sub>2</sub>-CO<sub>2</sub> mixtures through a convergent-divergent nozzle. In this technique the temperature dependence and magnitude of the relaxation rates can be varied until the N<sub>2</sub> vibrational temperatures predicted by the numerical solution agree with the measured temperatures. (See ref. 7.)

Since the gasdynamic laser using rapidly expanding  $N_2$  and  $CO_2$  has been shown to be practical (ref. 8), a knowledge of the mechanism of vibrational energy transfer within the modes of the various molecules and the rates that govern these transfers is necessary for prediction of laser performance. These rate processes are also important in nonequilibrium-flow calculations for vehicle entry into planetary atmospheres.

## SYMBOLS

$E$	vibrational energy
$H$	enthalpy
$M$	collision particle
$N_2^+B^2\Sigma_u$	excited ion state of $N_2^+$
$N_2X^1\Sigma_g$	ground state of $N_2$
$N_2^+X^2\Sigma_g$	ground state of $N_2^+$
$p$	pressure
$T$	temperature
$t$	time
$v$	vibrational quantum number
$x$	distance downstream on center line of nozzle
$X$	mole fraction
$\nu_1$	symmetric stretching mode
$\nu_2$	bending mode
$\nu_3$	asymmetric stretching mode
$\tau$	vibrational relaxation time

$\tau_A, \tau_B, \tau_C$  vibrational relaxation times illustrated in figure 1

Subscripts:

I,II modes of  $N_2$ - $CO_2$  vibrational model

t total

v vibrational state

Superscripts:

e equilibrium

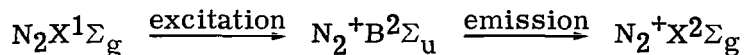
\* excited state

## EXPERIMENTAL METHOD

This investigation was carried out in the Langley 1-foot hypersonic arc tunnel, illustrated in figure 2. Flowing  $N_2$  is heated as it passes through the magnetically rotated arc and it is then mixed with unheated  $CO_2$  in the stagnation chamber. The mixture flows through a 0.55-cm-diameter sonic throat and expands in a  $5^\circ$  half-angle conical nozzle to the test section. A vacuum system consisting of a five-stage steam ejector maintains a back pressure of 0.05 mm Hg (7 N/m<sup>2</sup>). The reservoir temperature is essentially constant for each test. Reservoir temperatures between 1500 and 4000 K were obtained for individual tests by changing the arc gap length with various outer electrodes and by varying the relative percentages of  $N_2$  and  $CO_2$ . For a constant mass flow rate, stagnation reservoir pressure varied from 5 to 10 atm (507 to 1013 kN/m<sup>2</sup>) for this temperature range. This pressure variation is included in the theoretical predictions. Reservoir enthalpy (and thereby temperature) was computed by the sonic-throat method. A calibration of this technique with a tube calorimeter which accepted the total gas stream flowing from the tunnel throat established the accuracy of the enthalpy determination within  $\pm 10$  percent, as shown in figure 3. An explanation of the sonic-throat method and a detailed description of the tunnel and calorimeter are available in references 9 and 10. High-purity-grade commercial nitrogen (99.9-percent pure) and carbon dioxide (99.8-percent pure) were used, and a previous experiment (ref. 11) showed that similar impurity levels did not affect the measured vibrational temperatures in an expanding flow.

The limitations and errors of the electron-beam technique for measuring  $N_2$  vibrational temperature have been discussed in references 12 to 15; therefore only the basic

concepts will be described here. In this method an electron gun produces a narrow column of electrons (15 kV) which passes normal to the flow and through the test section (fig. 2): These fast electrons excite a small number of the particle making up the flow, and the emission of light resulting from the transitions of these excited particles to lower energy states is observed spectrographically to determine the  $N_2$  vibrational temperature. For tests both with  $N_2$  and with the  $CO_2$ - $N_2$  gas mixtures, the first negative system of  $N_2^+$  dominates all other observed bands in the visible spectrum. The electron-beam excitation-emission path is given by



and is illustrated in figure 1. Relative intensity ratios of the total emission from the (0,1) and (1,2) bands of  $N_2^+$  determine the  $N_2$  vibrational temperatures. References 13 and 15 present an expression for this intensity ratio as a function of  $T_v$ , and its applicability is a direct result of the Franck-Condon principle (ref. 16). This principle states that the electron transition in the molecule is so fast relative to the intermolecular motion that the internal motion of the molecule does not have time to adjust. Consequently, the electron-beam-excited  $N_2^+$  spectra indicate the thermal distribution of the  $N_2$  ground state. Lifetimes of  $N_2^+$  emission bands have been measured and are in the range of  $10^{-8}$  second. Quartz windows allowed observation of the light emission from the  $N_2^+$  molecular ions along the beam path by means of a 1/2-meter spectrograph. Entrance and exit slits were adjusted so that the (0,1) and (1,2) bands of  $N_2^+$  were just resolved in the first order by using a photoelectric readout which was fed to a micromicroammeter with output displayed on a strip recorder.

Some bands of  $CO_2^+$  were observed, the strongest being located at 2883 and 2896 Å, but these bands were too weak for detailed resolution and therefore only the  $N_2$  data were analyzed. Measuring the  $N_2$  vibrational temperatures from relative band intensities by the electron-beam technique is synonymous with determining the relative populations of the  $N_2$  vibrational levels. These measurements taken in a relaxing flow of  $N_2$  can therefore be used to calculate the relaxation rate of  $N_2$ .

### VIBRATIONAL RELAXING GASES

For every vibrational level of  $N_2$  there is a corresponding near-resonant vibrational level of  $CO_2$  in the asymmetric stretching mode  $\nu_3$ . Therefore, in an expanding relaxing mixture of  $N_2$  and  $CO_2$ , competitive processes will be occurring to depopulate the upper  $N_2$  vibrational levels, and the observed relaxation time will be a net result of these exchanges. The vibrational-translational process between the  $N_2$  molecules in pure relaxing  $N_2$  was analyzed separately so that the competitive relaxing processes could be

evaluated in the mixtures. A relative rational model of the many vibrational-translational and vibrational-vibrational energy exchanges which occur in a  $N_2$  and  $CO_2$  mixture has been presented by Anderson (ref. 7) and shown in figure 1. This diagram includes only the vibrational energy levels of interest in this investigation. The collisional transition probabilities computed (ref. 5) and measured (ref. 2) for this system indicate not only the very fast, resonant vibrational energy exchange between the  $v = 1$  level of  $N_2$  and the (001) level of  $CO_2$ , but also a fast exchange between the (100) and (020) levels of  $CO_2$  due to Fermi resonance. Vibrational energy is also rapidly transferred among the lower excited levels of the degenerate mode  $\nu_2$  in  $CO_2$  because of the nearly equal spacing of these levels. Since these fast transitions tend to couple various energy levels, Anderson (ref. 7) grouped the participating levels into two modes (modes I and II in fig. 1) which are assumed to be in equilibrium within themselves but not with each other.

In reference 7 a time-dependent technique is used for a detailed solution of this model, with the assumption that the vibrational energies of each mode relax as a simple harmonic oscillator. Therefore,

$$\frac{d(E_v)_I}{dt} = \frac{(E_v)_I^e - (E_v)_I}{\tau_I} \quad (1)$$

and a similar equation applies for  $(E_v)_{II}$  with a relaxation time  $\tau_{II}$ .

The relaxation times  $\tau_I$  and  $\tau_{II}$  are averages which characterize the net rate of energy transfer into and out of modes I and II and are governed by the transitions shown in figure 1 with relaxation times  $\tau_A$ ,  $\tau_B$ , and  $\tau_C$ . These relaxation times are also averages based on collisions between  $CO_2$ - $CO_2$ ,  $CO_2$ - $N_2$ , and  $N_2$ - $N_2$  and are obtained from the "parallel resistance" mixture rule given in references 7 and 17:

$$\frac{1}{\tau_A} = \frac{X_{CO_2}}{\tau_A(CO_2-CO_2)} + \frac{X_{N_2}}{\tau_A(CO_2-N_2)} \quad (2)$$

Similar relations may be expressed for  $\tau_B$  and  $\tau_C$ . Two vibrational temperatures  $(T_v)_I$  and  $(T_v)_{II}$  are defined by using this model, where  $(T_v)_{N_2} = (T_v)_{II}$ . The distributions of the two vibrational temperatures along the nozzle center line are compared with the translational temperature distribution in figure 4 for conditions typical of this experiment. As shown, mode II, and therefore  $(T_v)_{N_2}$ , relaxes much slower than mode I, and neither mode I nor mode II is in equilibrium with the local translational temperature.

## RESULTS AND DISCUSSION

Vibrational temperatures of  $N_2$  were measured in expanded flows of pure  $N_2$  and mixtures of  $N_2$  and  $CO_2$  as a function of total temperature. The results obtained in pure

N<sub>2</sub> are shown in figure 5, along with curves of the predicted values of T<sub>v</sub> from the analytical program. Vibrational relaxation times used in computing the upper curve were taken from a line fitted to the shock-tube data for N<sub>2</sub> found in reference 2, and this distribution does not agree with the vibrational temperatures measured in the expanding N<sub>2</sub>. To evaluate the data of this report, the relaxation-time expression is assumed to have the well-known form

$$\tau p = A \exp(BT^{-1/3}) \quad (3)$$

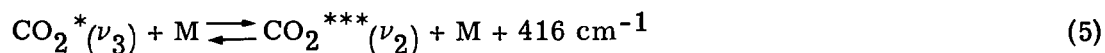
where p is the pressure and the constants A and B are evaluated by using the non-equilibrium program. The expression for  $\tau p$  that best fits the measured N<sub>2</sub> vibrational temperatures of figure 5 is

$$\tau p = 3.4 \times 10^{-12} \exp(195T^{-1/3}) \text{ atm-sec} \quad (4)$$

Vibrational relaxation times of N<sub>2</sub> observed in expanded flows are known to be less than predicted by the theory or measured in shock tubes (ref. 18), and several explanations for this difference are offered in references 19 to 21.

The analysis of the N<sub>2</sub>-CO<sub>2</sub> mixture is somewhat more complicated in that six vibrational relaxation expressions must be considered. There are two expressions each for  $\tau_A$ ,  $\tau_B$ , and  $\tau_C$ ; one expression is for collisions with like molecules and the other for collisions with unlike molecules. (See fig. 1.) The relaxation time  $\tau_B(\text{N}_2\text{-N}_2)$  evaluated for expanding N<sub>2</sub> and given by equation (4) is used for analyzing the mixture and because of a lack of reliable data showing any significant difference (ref. 2),  $\tau_B(\text{N}_2\text{-CO}_2)$  is set equal to  $\tau_B(\text{N}_2\text{-N}_2)$ . The relaxation rate of the CO<sub>2</sub> transition (000)  $\rightarrow$  (010) has been measured, by a number of techniques, for collisions with both CO<sub>2</sub> and N<sub>2</sub>, and the results indicate that CO<sub>2</sub> is 4 times as effective as N<sub>2</sub> in this energy transfer process. (See ref. 2.) However, no measurements have been made of these relaxation times in an expanding flow. Therefore the values predicted by the Schwartz, Slawsky, and Herzfeld (SSH) theory are used for  $\tau_C(\text{CO}_2\text{-CO}_2)$  and, as indicated in reference 2,  $\tau_C(\text{CO}_2\text{-N}_2)$  is assumed to be equal to  $4\tau_C(\text{CO}_2\text{-CO}_2)$ . The difference in these relaxation rates is not critical to the present measurements because both the measured and predicted times  $\tau_C$  are so much less than either  $\tau_A$  or  $\tau_B$  that the vibrational temperatures of the N<sub>2</sub>, and therefore the relaxation time  $\tau_A$ , will not be affected.

The greatest uncertainty lies in the selection of the values of  $\tau_A$ , and the evaluation of these times is the primary purpose of this experiment. Taylor and Bitterman (ref. 2) assume that the  $\nu_3$  and  $\nu_2$  modes of CO<sub>2</sub> are coupled through the mechanism described by





and most of the data presented by them indicate a rate from 10 to 100 times faster than that predicted by the SSH theory (ref. 5). Furthermore, the efficiency of  $\text{CO}_2$  as a collision partner in this reaction is seen to be 2 to 3 times that of  $\text{N}_2$ .

The vibrational temperatures of  $\text{N}_2$  measured in three mixtures of  $\text{N}_2$  and  $\text{CO}_2$  are shown in figures 6, 7, and 8, along with curves of the values of  $T_v$  predicted by using Anderson's model of relaxation in an expanding flow (ref. 7). The upper curve in figure 6 was computed by using the rates given in reference 2, which are based largely on shock-tube data, and this curve does not agree with the measurements in the expanding flow. The distributions of vibrational relaxation time which predicted the measured values of  $(T_v)_{\text{N}_2}$  are shown in figures 6, 7, and 8, and these predictions are seen to be consistent for gas mixtures of 10.8 to 30 percent  $\text{CO}_2$  in  $\text{N}_2$ . To obtain the proper predictions, the  $\tau_A$  values are varied from the SSH predictions until a distribution is found to fit the data. The relaxation times  $\tau_A$  are found to be 1/100 as long as predicted by the theory. They are in general agreement with the data of reference 2, although somewhat shorter. The  $\tau_A(\text{CO}_2\text{-CO}_2)$  times are set at 0.27 those of  $\tau_A(\text{CO}_2\text{-N}_2)$ , as indicated in reference 2. The SSH values referred to for  $\tau_A$  are taken from reference 5, where Herzfeld calculated the rates for the collisional deactivation of mode  $\nu_3$  of  $\text{CO}_2$  for a large number of possible vibrational-vibrational mechanisms. The rate used is the overall rate which is the sum of all these processes. Dissociation and recombination are not considered in the analysis of these measurements, although  $\text{CO}_2$  dissociation would have some significance for the high-temperature data. A decrease in the  $\text{CO}_2$  concentration should result in an increase in the effective relaxation time, and therefore an increase in the vibrational temperatures. The higher temperature data of figures 6, 7, and 8 appear to show this effect.

## CONCLUDING REMARKS

The vibrational relaxation rates for expanding mixtures of  $\text{N}_2$  and  $\text{CO}_2$  were evaluated by using the electron-beam technique and a time-dependent method for the solution of nonequilibrium flow. The results show that the vibrational relaxation rate between the asymmetric stretching mode  $\nu_3$  and the bending mode  $\nu_2$  of  $\text{CO}_2$  is 100 times as fast as predicted by the Schwartz, Slawsky, and Herzfeld (SSH) theory. The specific processes that cause the discrepancy in these rates are not known, but the very fast relaxation times indicate near-resonant reactions. Since the SSH prediction is an overall evaluation of all the known transitions between the  $\nu_3$  and  $\nu_2$  modes, the theory appears inadequate to

explain the complex mechanism for intramolecular vibrational-vibrational energy transfer in polyatomic molecules.

Langley Research Center,  
National Aeronautics and Space Administration,  
Hampton, Va., August 20, 1971.

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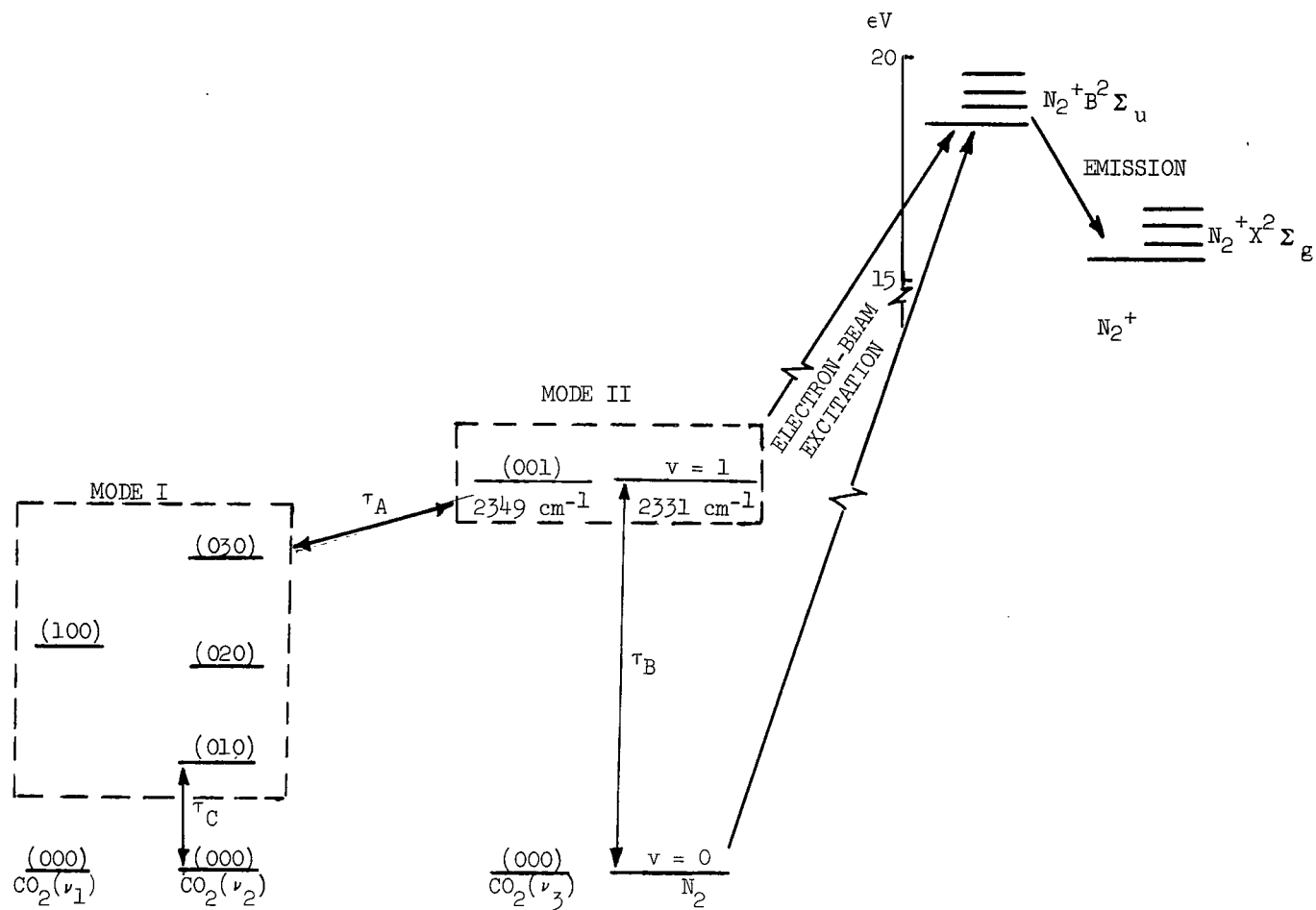


Figure 1.- Partial energy-level diagram for  $\text{CO}_2$ ,  $\text{N}_2$ , and  $\text{N}_2^+$  showing transitions important to the experiment.

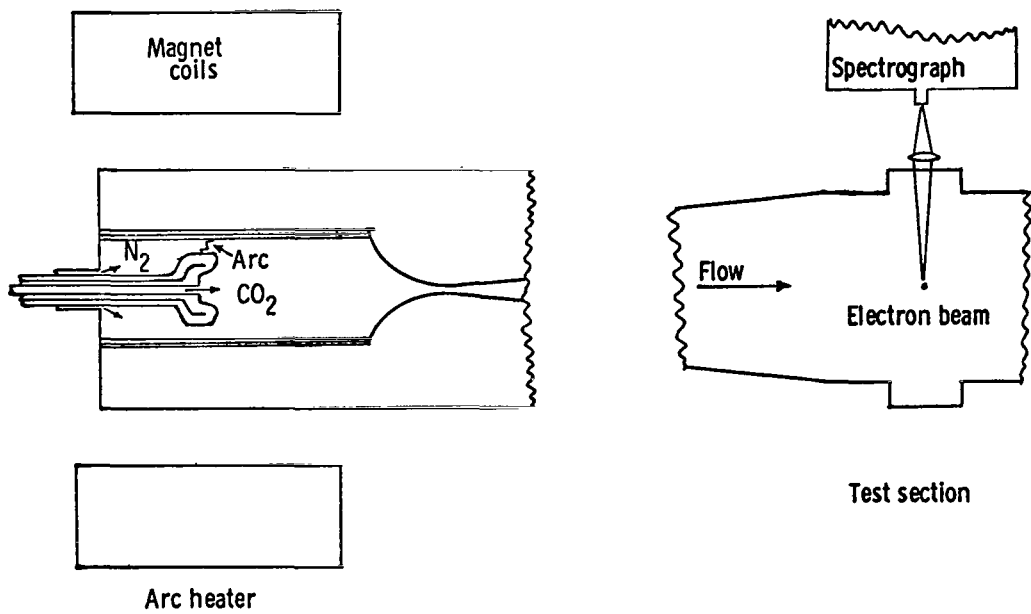


Figure 2.- Sketch of experimental apparatus and method used to inject gases into arc heater.

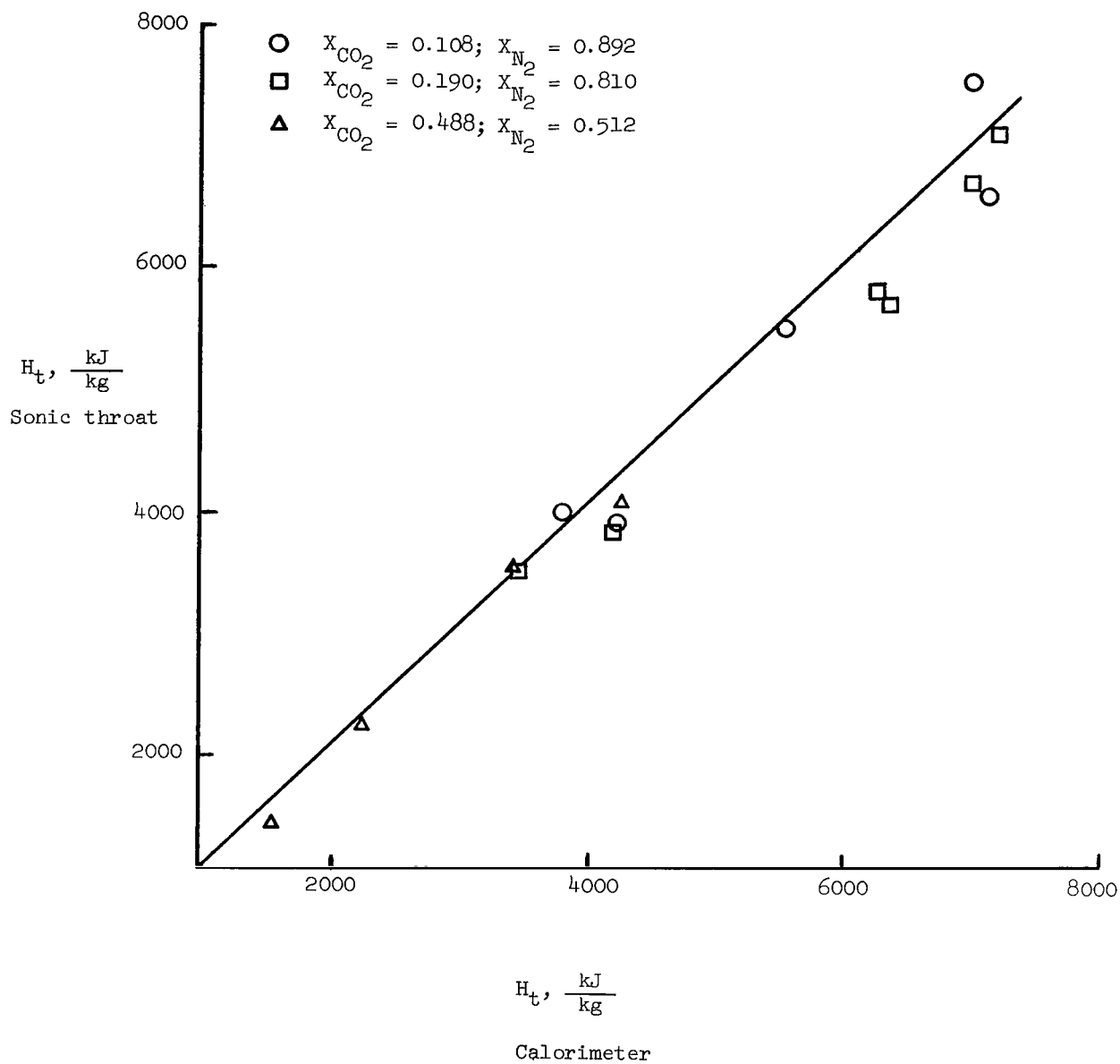


Figure 3.- Correlation of total enthalpy as determined by the sonic-throat method and by means of a calorimeter.

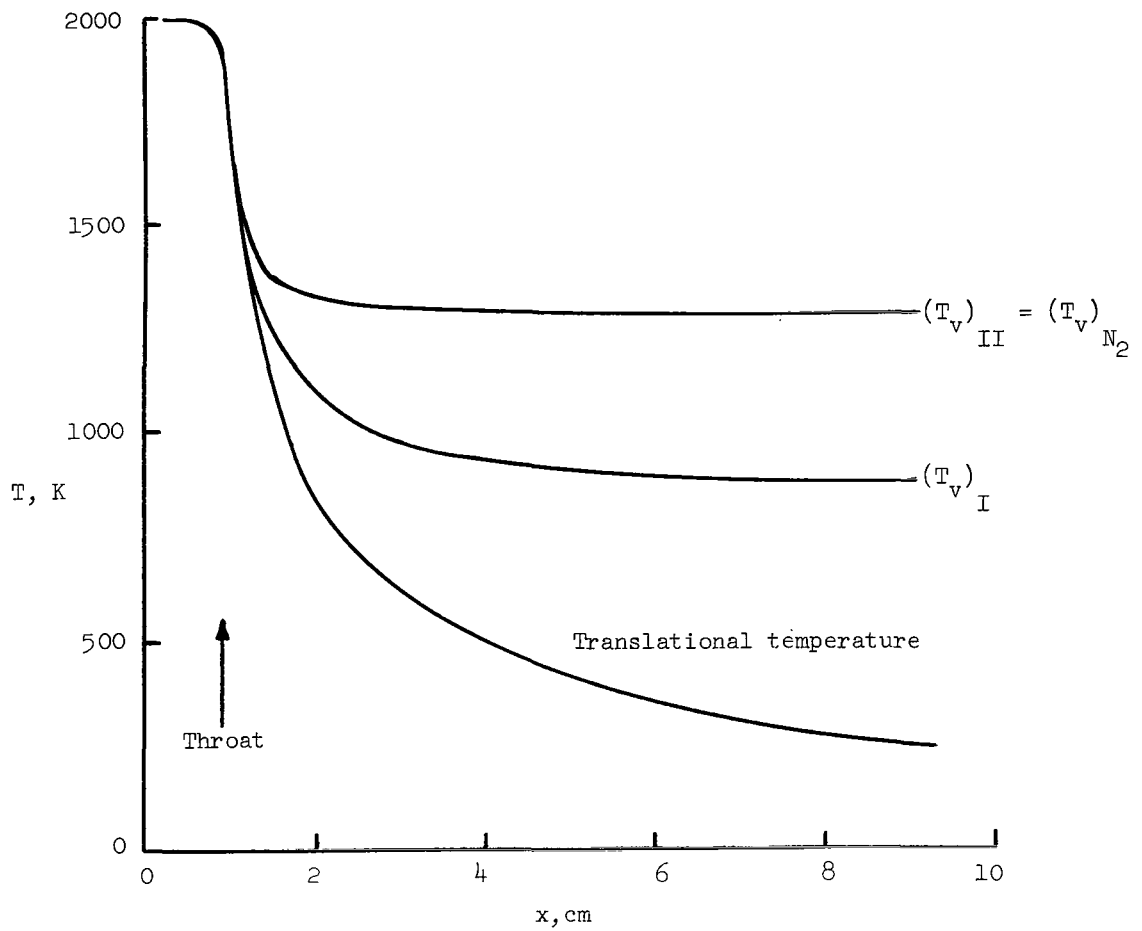


Figure 4.- Vibrational and translational temperature distributions through the nozzle for a mixture of  $X_{CO_2} = 0.108$  and  $X_{N_2} = 0.891$ .  $T_t = 2000$  K;  $p_t = 5.8$  atm.



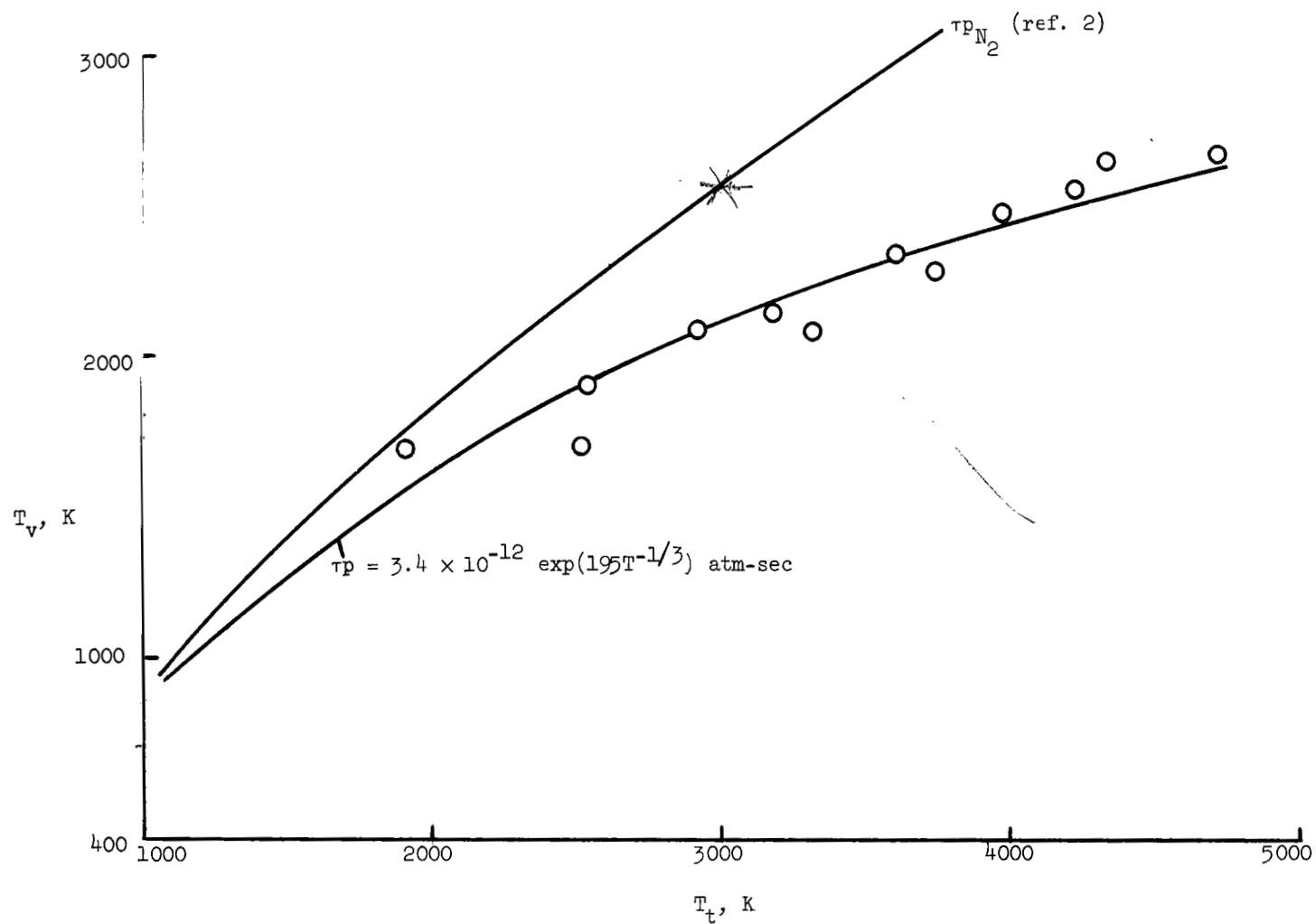


Figure 5.- Measured and predicted  $N_2$  vibrational temperatures as a function of total temperature in pure  $N_2$ .

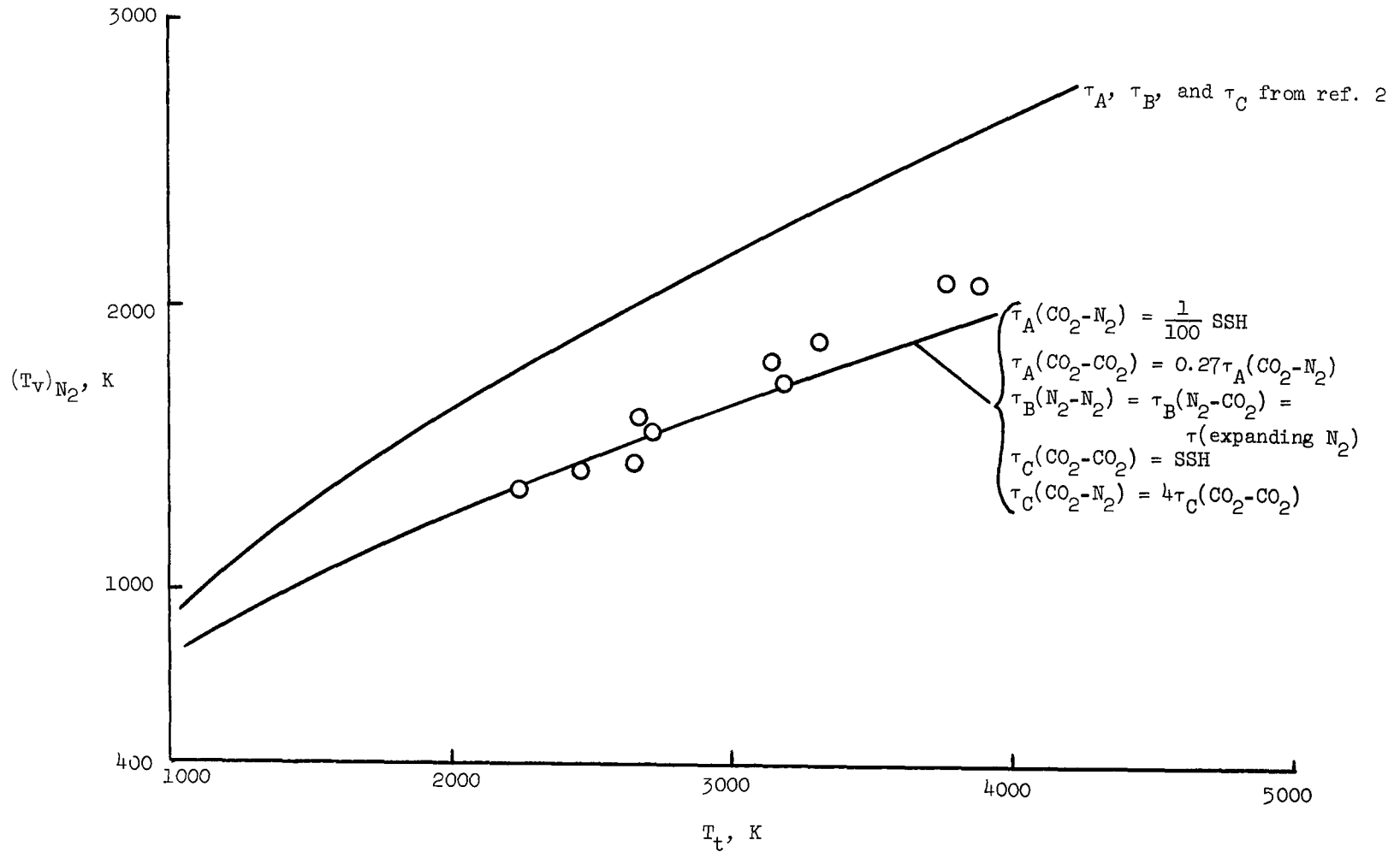


Figure 6.- Measured and predicted  $\text{N}_2$  vibrational temperatures as a function of stagnation temperature in a mixture of  $X_{\text{CO}_2} = 0.108$  and  $X_{\text{N}_2} = 0.892$ .

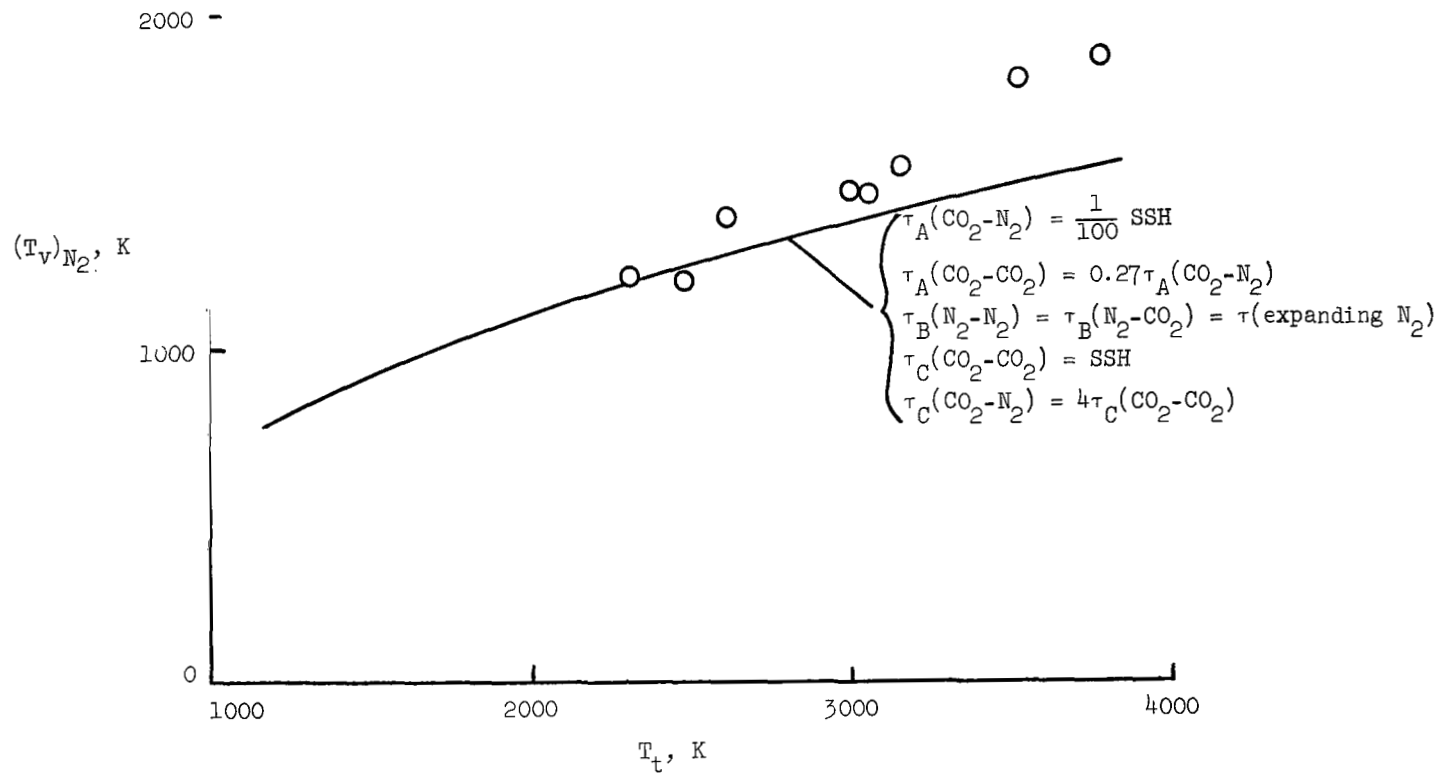


Figure 7.- Measured and predicted  $N_2$  vibrational temperatures in a mixture of  $X_{CO_2} = 0.190$  and  $X_{N_2} = 0.810$ .

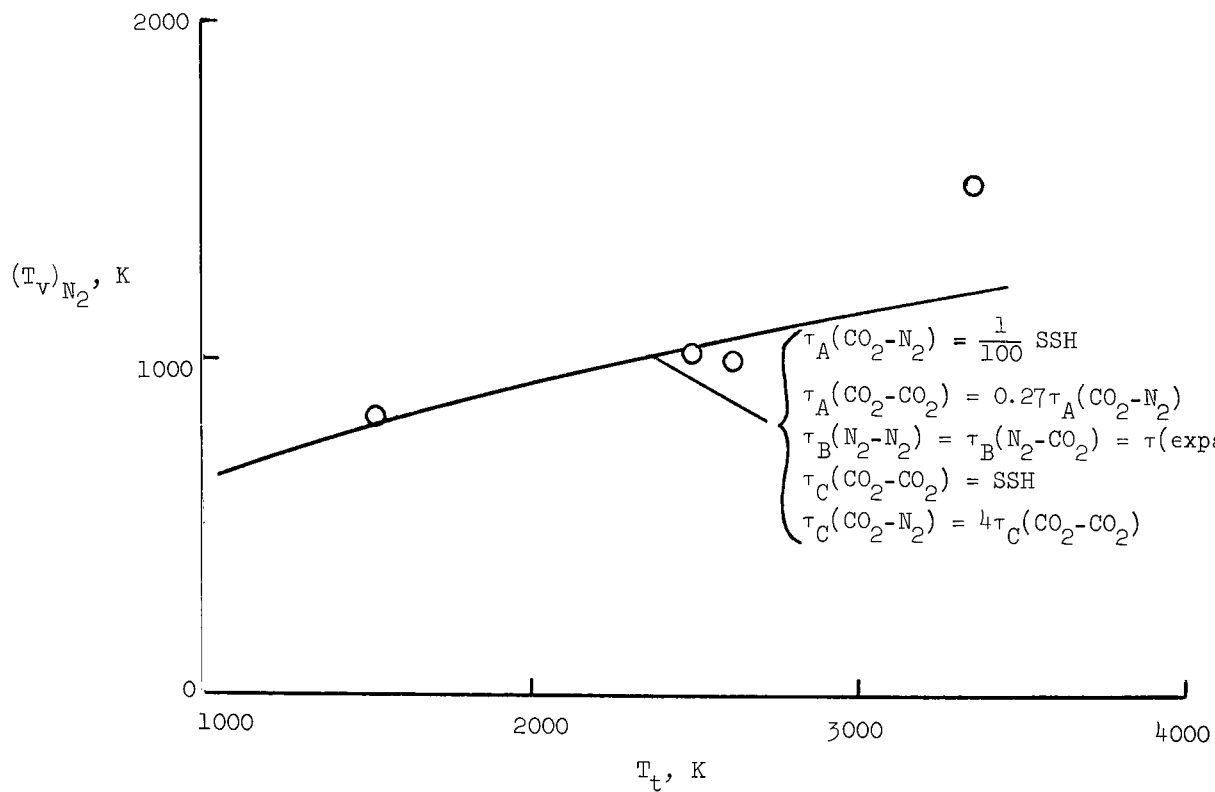


Figure 8.- Measured and predicted  $N_2$  vibrational temperatures in a mixture of  $X_{CO_2} = 0.300$  and  $X_{N_2} = 0.700$ .



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